



### Lacrosse

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### OFTPATION REDWING

A PRELIMINARY REPORT

OF

Submitted by Task Group 7.1

5005JFE

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5 July 1956

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### INTRODUCTION

This is a proliminary report, and therefore, does not give either complete or final results of the work of the various projects. No information on the construction of the device is included, in order that the classification may be kept to Secret Restricted Data.

The DELETER device was detonated on the north end of Runit Island, Eniwetok Atoll, at 0625:29.8, May 5, 1956, local time, as a ground shot. []][[]] was designed as an externally initiated, [][[]]

Therefore, the diagnostic experiments included measurements on fireball yield, radiochemical yield, external neutron threshold detectors, alpha transit time, performance of the ENS units, etc. Escause of its applied yield, the device was also used as an energy source DELETED DELED

to determine nuclear vulnerability of stock

pile capons, and a variety of weapon effects tests.

This upport gives results of the work of Task Units 1, 3, and 4. The work of other Task Units was either in support of the units mentioned, or concerned with the detonation of the device, and will be described in other reports.

The yield was about 39 KT, approximately as predicted,

# DELETED

and optical brightness experiments worked Thel well, as did the various effects measurements.

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GENERAL INFORMATION

Costoved Weather at Shot Time Dunit Island - Scientific Stations and Zero Point Fro - and Fost Shot Photos RedSafe Surveys at H / 8, D / 1, and D / 2





### INTWITCK CESSIEVED WEATHER FOR 5 MAY 1956 LACROSSE SHOT TIME 0625M

| Sea Level Pressure | 1003.5 mb                 |
|--------------------|---------------------------|
| Temperature        | 81°F                      |
| Dew Foint          | 77°F                      |
| Relative Humidity  | इ <b>!;%</b>              |
| Surface Wind       | 030 <sup>°</sup> , 16 kts |
| Visibility         | More than 10 miles        |

### CLOUDS

1/10 cumulus, bases 1,500 feet, tops 4,000 feet; 1/10 altostratus, **bases** 18,000 feet, tops 19,000 feet; 5/10 cirrostratus, bases 43,000 feet, tops 44,000 feet. (Cloud bases and tops reported by eineraft)

There ware no charars or other precipitation within 50 dies of Reivicok.

Enivetok Ingoon:

Average of highest 1/3 of traves 1.5 feet on cast side of lagoon in.

Coon Sea:

Average of highest 1/3 of these 4.5 to 6 feet, direction 030°.

ETITATION SOULDING

|    | Pressure<br>Millibara | Height<br>Feet                        | Carporature .<br>OC | Dow Point |
|----|-----------------------|---------------------------------------|---------------------|-----------|
|    | 1008                  | Sfc                                   | 27.2                | 23.8      |
|    | 1000                  | 250                                   | 26.4                | 23.4      |
|    | 910                   |                                       | 20.2                | 18.8      |
|    | 850                   | 1.890                                 | 18.1                | 09.2      |
|    | 811                   | · · · · · · · · · · · · · · · · · · · | 1.7.3               | 02.5      |
| p? | 700                   | 10.270                                | 09.5                | -12.5     |
|    | 662                   |                                       | 06.2                | -15.8     |

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| Pressure<br>Millibars | Heigh <b>t</b><br>Fee <b>t</b> | Temperature<br>C                       | Dew Point     |
|-----------------------|--------------------------------|--|---------------|
|                       |                                |  |               |
| 611                   |                                | 02.2                                   | -01.8         |
| 600                   | 14.400                         | 01.8                                   | -09.8         |
| 500                   | 19,140                         | -09.2                                  | -12.2         |
| 1.1.5                 |                                | -13.2                                  | -29 <b>.2</b> |
| 200                   | 21 720                         | -17.5                                  | М             |
| 31.5                  |                                | -26.2                                  | -39.8         |
| 211.                  |                                | -30.8                                  | -36.8         |
| 200                   | 31 580                         | -33.2                                  | -39.2         |
| 270                   | 000                            | -38.5                                  | -1;4.2        |
| 200                   | 10 530                         | -55.0                                  | М             |
| 200                   | 46,360                         | 59.8                                   | М             |
| 104                   | 0000                           | ······································ | м             |
| 100                   | 53 960                         | 79.2                                   | М             |
| 100                   | 900 e C C                      | -76-0                                  | М             |
| 078                   |                                | -70.0                                  | М             |
| 050                   |                                | -71.0                                  | М             |
| 059                   | 67 200                         |  | М             |
| 050                   | 070                            |  |               |
| 014                   |                                |  |               |

:

### ENTWETOK WINDS ALOFT

| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | Height   | Direction  | Speed   | Height   | Direction   | Speed   |
|---|--|--|---|--|---|---|
|   | Fost   | Degrees  | Knot <b>s</b>   | Foet   | Degrees   | Y abs   |
| ≤⊃, >>0 2/,0 ±3                                       | 5 rface<br>1,000<br>2,000<br>3,000<br>3,000<br>5,000<br>6,000<br>7,000<br>8,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,000<br>10,00 | 030<br>100<br>110<br>110<br>110<br>100<br>100<br>100 | 15<br>24<br>24<br>25<br>29<br>30<br>28<br>23<br>20<br>20<br>11<br>5<br>4<br>4<br>13 | 25,000<br>30,000<br>35,000<br>40,000<br>50,000<br>55,000<br>60,000<br>65,000<br>65,000<br>75,000<br>75,000<br>85,000<br>85,000<br>90,000<br>94,000 | 260<br>240<br>260<br>240<br>240<br>240<br>230<br>130<br>130<br>130<br>130<br>130<br>130<br>130<br>130 | 24<br>37<br>52<br>60<br>59<br>61<br>39<br>61<br>39<br>8<br>13<br>10<br>28<br>42<br>56<br>57 |

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PART II

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TABE UNIT 3

DOD PROTRACS

K.D. Coleman Osl. K.D. Coleman OTU-3

Program 4 - Bicandical Effects It Col C. W. Bankos Program 5 - Aircraft Structures CDE M.R. Dahl Program 6 - Test of Service Equipment and Materials It Col C. W. Bankes CDR A.H. Higgs Maj. W.C. Linton Program 8 - Thermal Radiation and Effects Lt Col J.G. James Program 9 - General Support

- 14 -



#### I LOBIDSD

Project 1:1 - Basic Blast Measurements - J.J. Meszaros

### CERECTIVES

The primary objective of Project 1.1 in the LACRO33E participation was to measure air blast pressure and dynamic prossure at various distances along a blast line. From the pressure time records it was to be determined whether a precursor was formed from this size device detonated on the surface.

A secondary objective was to furnish Project 1.5 with dynamic pressure at the various locations of the jeep stations.

### JUSTAU TULTION

The BRL self-recording pressure-time and "q" gages were used to record the air blast and dynamic pressure. The air blast gages are installed at surface level and the "q" gages are mounted at a height of 3 feet from the surface.

### THEVELTS

There were 15 pressure-time gages installed. Two of the 15 initiated prematurely giving a peak pressure only.

Fine sand tended to clog the pressure inlet hole and to prevent this a piece of carbon paper was taped over the hole. The paper burned off at stations out to a distance of 3350 feet. Beyond this distance the record shows a slow rise in pressure indicating the pressure inlet hole was clogged with sand or paper.

The results of the shot are presented in TABLE 1.1-1



| - |  |
|---|--|

### TABLE 1.1-1

|        | Distanc <b>e</b> |   | Peak<br>Pressure | Duration        | Arrival<br><u>Tim</u> e |
|--------|------------------|---|------------------|-----------------|-------------------------|
| 114.15 | 1180             |   | 121.8            | •340            |                         |
| 115.22 | 1590             |   | 138.0<br>55.9    | <b>Feak</b>     | - <b>199</b>            |
| 115.23 | 1950             |   | 36.2             | .531            | .316                    |
| 115.24 | 2500             |   | 19.8             | .579            | .650                    |
| 114.16 | 2770             |   | 15.6             | .719            | 1.007                   |
| 115.25 | 3350             |   | 10.4             | .672            | 1.301                   |
| 115.31 | 3900             |   | 3.7≭             |                 | 1.504                   |
| 114.18 | 4378             |   | 3.9*             | •94 <b>9</b>    | 2.007                   |
| 115.26 | 5200             |   | 3.1*             | 1.043           | 3.11.2                  |
| 115.26 | 5200             |   | 4.6              | Peak            |                         |
|        |                  |   |                  | Peak Dynasic    |                         |
| 115.22 | 1590             | ť | 150.0 *          | 94 <b>.</b> 0 * |                         |
|        |                  | 5 | 55.0             |                 |                         |
| 115.23 | 1950             | t | 52.0             | 13.0            |                         |
|        |                  | S | 34.0             |                 |                         |
| 125.24 | 2500             | t | 27.2             | 7.2             | •<br>•                  |
|        |                  | s |                  |                 |                         |
| 115.25 | 3350             | t | 13.0             | 2.1             |                         |
|        |                  | s | 10.9             |                 |                         |
| 115.31 | 3900             | t | 9.3              | 1.1             |                         |
|        |                  | s | 8.2              |                 |                         |
| 115.26 | 5200             | t | 5.8              | 1.0             |                         |
|        |                  | s | 4.8              |                 |                         |

\* Pressure values obtained are questionable.

t is total pressure, s is static pressure.

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### LACROSSE

## Froject 1.2 - SURFACE PLAST MEASURIMENTS OF STATIC AND DYNAMIC PRESSURES - A. D. Thornbrough

Carter D. Broyles

This experiment was designed to measure overpressure and dynamic pressure vs time from a surface burst of a medium yield (40 KT) nuclear explosion. Overpressures were measured with gages in ground baffles and pitot-static tubes. Dynamic pressures were measured with the pitotstatic tube mounted 3 feet above the ground surface.

The overpressures and dynamic pressures are in general agreement with previous measurements of a 1 KT and of megaton bursts, being consistent with  $W^{1/3}$  scaling and a reflection factor of 1.6 using a freesir pressure distance curve. However, a precursor of limited extent disted in the high pressure region (120-50 psi). It is expected that for more favorable conditions, that is, a low mass weapon and dry ground, the greeness would be more extensive.

The detailed results are given in the tables and graphs.



| OLEARTISSURE RESULTS |  |
|----------------------|--|
| 1-2-1                |  |
| TALLE                |  |

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| STATION | GROUND<br>RANGI                     | CAGE   | ARRIVAL<br>TIME                        | PEAA<br>POSITIVE<br>PRESSURE                 | PEAK<br>NEGATIVE<br>PRESSUE        | POSITIVE<br>PRESSURE<br>DURATION | NEGATIVE<br>PRESSURE<br>DURATION | POSITIVE<br>PRESSURE<br>DAPUISE | SELUCION DE CONTRAL<br>ENUSSITA<br>MULLSU |
|---------|-------------------------------------|--|--|--|------------------------------------|----------------------------------|----------------------------------|---------------------------------|---|
|         | (N)                                 |  | (aec)                                  | (psi)  | (psi)                              | (sec)                            | (360)                            | (psi-sec)                       | (ps1-sec)                                 |
| 3021    | 069                                 | <b>J</b> GBL                                 | 0.050                                  | 425  | Record ba                          | d after 0.058                    | 3 sec                            |                                 |   |
| 3021    | 690                                 | lCBR   | 0.050                                  | 375  | Record ba                          | d after 0.05/                    | + 30C                            |                                 |   |
| 3021    | 069                                 | 1GBR-RF                                      | 0•050                                  | 320  | Record ba                          | d after 0.090                    | ) sec                            |                                 |   |
| 3022    | 920                                 | 2CBL   | <b>701.</b> 0                          | 160  | Θ                                  | 0.48                             | Ð                                | 8.4                             | C   |
| 3022    | 920                                 | 2GDR   | 0.102                                  | 135 <sup>a</sup>                             | Record ba                          | d after 0.11                     | 3 360                            |                                 |   |
| 3023    | 1368                                | 3P3  | 0.244                                  | 69 <sup>b</sup>                              | 4•3                                | 0**0                             | 4•5                              | 4.5                             | 3 <b>-</b> 01                             |
| 3023    | 0071                                | 3GHL   | 0.248                                  | 55 <sup>c</sup>                              | 3.7                                | 0**0                             | 4•3                              | 5.7                             | 5.7                                       |
| 3023    | 0071                                | 36111  | 0.264                                  | 56 <sup>d</sup>                              | 2.5                                | <b>7•0</b>                       | 3.5                              | 5.2                             | 5.9                                       |
| 120.01  | 1793                                | Eatoo  | 0.447                                  | 34   | 4.0                                | 0.5                              | 4.4                              | 4.                              | 7.5                                       |
| 3024    | 1825                                | 4GEIL  | 0.462                                  | 34   | 5•5                                | 0.5                              | 4•5                              | 3.5                             | 12.5                                      |
| 3024    | 1825                                | 4 GBR  | 0.464                                  | 35   | 3.0                                | 0.53                             | 4.4                              | 5.2                             | 6•9                                       |
| 120.02  | 2500                                | <b>002</b> P3                                | 143.0                                  | 16.9   | 2.1                                | 0.62                             | 4.3                              | 3.0                             | 2.8                                       |
| 121.01  | 2500                                | 10108  | 0.842                                  | 18.4L  | 1.B                                | 0.80                             | 3.9                              | 3 <b>.</b> 6                    | 3.4                                       |
| 120.03  | 2900                                | E4E00  | ī.• 096                                | 12.8   | 1•7                                | 0 <b>.</b> ይկ                    | 0•1                              | 3.4                             | 2.5                                       |
| 121.02  | 2900                                | 10203  | 1.097                                  | 13.0   | 1 <b>.</b> 8                       | 0.79                             | 4.4                              | 3•4                             | 3.6                                       |
| 120.04  | 3250                                | Eat100                                       | 1.330                                  | 10.9   | л•3                                | 0.87                             | 4•6                              | 3.0                             | 4.6                                       |
| 5 0 5   | oak presu<br>eak presu<br>eak presu | ure at 0.110<br>ure at 0.268<br>ure at 0.292 | sec, initi<br>sec, precu<br>sec, precu | tal rise 160<br>irsor pressu<br>irsor pressu | psi.<br>ra 14.9 psi.<br>re 23 psi. | 9                                | . Peak pres                      | ssure at 0.25<br>ble.           | 6 Bec.                                    |

Foak pressure at 0.110 sec, initial rise 100 psi. Peak pressure at 0.268 sec, precursor pressure 23 psi. Peak pressure at 0.292 sec, precursor pressure 23 psi.

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| STATION      | GROUND<br>RANGE   | GÁŒE   | ARRIVAL<br>TIME | PEAK<br>DYNAMIC<br>FRESSURE           | DYNAMI <b>C</b><br>FRESSUR <b>E</b><br>DURATION | DYNAMIC<br>PRESSURE<br>IMPULSE |
|--------------|---|--|-----------------|---------------------------------------|---|--------------------------------|
| a            | (ft)  | and and an | (sec)           | (psi)                                 | (sec)   | (psi-sec)                      |
| 302 <b>2</b> | 92 <b>0</b>   | 293  | 0.104           | 265                                   | 0,12  | 7.0                            |
| 302 <b>3</b> | 136 <b>8</b>  | 303  | 0,21,4          | 180 <sup>a</sup>                      | 0.78  | 7.3                            |
| 120.01       | 1795  | 001 <b>03</b>                                  | 0.446           | 23                                    | 0.23  | 2,2                            |
| 121.02       | 2500  | 002q <b>3</b>                                  | 0.840           | 6.9                                   | 0.67  | 0.93                           |
| 120.03       | 290 <b>0</b>  | 0030 <b>3</b>                                  | 1.096           | 4.1                                   | 0.9   | 0.86                           |
|              | antaga saban ka maga ng pangang pang ng kara ta karabka |  |                 | · · · · · · · · · · · · · · · · · · · |   |                                |

TABLE 1.2-2 DYNAMIC FRESSURE RESULTS

a. Peak pressure at 0.110 sec, initial rise 100 psi.

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> DETAIL OF GAGE STATIONS STATIONS NOT ON SAME RADIAL LINE.

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### TACROSSE

Project 1.3 - SHOCK PHOTOGRAPHY - J. Fetes

### OFJECTIVES

The objectives for this shot were as follows:

1. To study the mechanical effects of a water surface on shock propagation.

2. To study the thermal effects, if any, resulting from the heating of air near the ground surface on shock transmission.

3. To determine peak shock overpressure as a function of distance both at the surface (water) and above ground zero.

### TNSTRUMENTATION

The instrumentation for this shot included both smoke rocket photo-

The rockets were fired from a station on the reaf, 3,000 feet NW of 3.000 zero. Causras were located on the south end of YVONNE and at the flock to er.

### . SULTS

The rocket instrumentation was successful and three films of good quality were obtained from the photo station on the south and of WOME. These films will be usable for the determination of peak shock overpressure (objective 3) and for a study of the mechanical effects of a water surface on shock propagation (objective 1).

As the result of a power failure on the Mack tower, no films were obtained. Consequently, a study of thermal effects on this shot is impossible (objective 2).

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### **JACRODSE**

### Troject 1.5-1 Drag Characteristics of various shapes - Vehicle Damage Effects - J.J. Meszaros

### OBJECTIVE

To compare the damage of this detonation to Shot 2 of Operation TEAPOT. It seems that the vehicle damage from Shot 2 **DELETED** as greater than expected. The exposure of vehicles to Shot LACROSSE is an effort to check damage prediction for this size weapon.

#### TECHNIQUES

Ten vehicles, truck, 1/4 ton 4x4 utility, WW II Model MB were arranged in pairs at five stations from GZ. The stations were 2500, 2770, 3350 3900, and 4378 feet from GZ. One vehicle at each station was oriented with the front facing GZ (face-on) while the side of the other vehicle was toouds GZ (side-on). Steel stakes were driven in the ground at each whicle station to facilitate displacement measurements.

#### RESURTS

Evaluation of the damage revealed underste damage to the side on whiches at the 2500 feet and 2770 feet station. The damage to all other vehicles was considered light damage. Six of the latter vehicles were considered immediately combat uscable requiring no maintenance other than filling with fuel, water or battery acid while the other two vehicles sustained a broken oil line and bent steering shaft and column. The face on vehicles remained upright. Five of the side-on vehicles were overturned; four upside down and one on its left side.

Displacement for the face-on vehicles ranged from 33' at the forward station to one foot at the most distant station. The side-on vehicles displacement ranged from 123 feet to 9 feet respectively.

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No prices thereal effects were noted offer then scorched paint and seats. Static pressure effects observed included partially collapsed fuel tanks and tool compartments at the two closest stations.

In general the damage was less than expected when compared to probability damage as obtained from the formulae and curves of 1M23-200. One contributing factor to the lighter damage was the soft candy soil at the vehicle stations. Complete explanation for the reduced damage is not fully apparent and conclusions from this shot will have to avait thorough analysis of pressure records.

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### LACROSSE

Project 1.6 - DRAG LOADING ON MODEL TARGETS - J. Petes

The U. S. Naval Ordnance Laboratory participated in Operation REDWING on Shot LACROSSE with a project designed to study drag force loading on model targets. Two and three component force gages were used with test models of cylindrical, parallelepiped, cubical, and spherical shapes. Shot LACROSSE, approximately 40 KT yield device, was detonated at the ground surface and produced at the distances of interest, 2,500 feet and 5,200 feet from ground zero, essentially clean, Mach shocks with negligible precursor, thermal, or dust disturbances. At these distances, side-on over-prescurs and dynamic pressures of 18.1 psi and 6.1 psi, and 4.5 psi and 0.47 psi respectively, were massined by this project.

All instancestation operated obtained on plote drag for c, time histories were obtained from all gages. Good correctent was obtained in cave shapes and amplitudes between similar gages at a clotion, thus establishing a high confidence level in the reproducibility of the gages and reliability of the data. The stingless configurations of cubes mounted on ground planes, and cylinders and parallelepipeds gave highly reproducible tesults and reasonable drag coefficient values. The  $C_D$ 's for these models did not vary significantly between the high q and low q regions;  $C_D$  values obtained were 1.0 for the 4" cubes, 0.37 for the 6" diameter cylinders, and 1.38 for the 6" x 6" cross-section parallelepipeds.

The spherical models mounted on stings did not produce data readily interpretable. Drag coefficients at the low q region were higher by a factor of two than the  $C_D$  values at the higher q region. Results similar to this



The full evaluation of LACROSSE results await the completion of a laboratory drag study, further study of the LACROSSE data obtained by this project and by other projects, and full evaluation of data. This will be accomplished in the final report.

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### LACROSSE

Froject 1.8 - CRATER MEASUREMENTS - Captain F. E. Deeds

### CEJECTIVES

The objective of this project was to measure the physical characteristics of the crater produced by detonation of an atomic weapon at ground surface. A further objective was to correlate data obtained with previous surface bursts at the Pacific Proving Grounds (PPG) and with the JANGLE surface shot at the Nevada Test Site. The crater is an important effect of a nuclear detonation when used on hard targets or underground complacer as. A thercugh understanding of this phenomena is necessary to predict proper ucage to achieve the desired results.

UNSTRUMENTATION OR TECHNIQUES

Preshot Survey: Rays extending from ground sero and 60 digited apart were surveyed to a distance greater than the expected crater radius (Fig. 1.8.1). The elevations found varied from 0.3 to 2.2 feet above the datum plane (6 inches below mean-low-water springs) for distances out to 450 foot from ground zero. Uncontrolled stereoptic aerial photographs were taken of the shot area.

Postshot Survey: Aerial photographs were taken at H / 2 to usasure creater diameter with stereoptic equipment. Depth of the creater, above water surface, can also be measured by the same means. A USAF RB-50 E aircraft equipped with a USAF Aerial mapping Camera, T-11, having a 6-inch-focallength lens was used to make the mapping runs. The camera was gyroscopic stabilized mounted and the intervalometer was set for a forward overlap of 57 to 62 percent. The aerographic film was developed at the PPG to insure proper coverage of the target and sent to the Engineer Research and

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Development Inboratories for analysis. The aircraft was equipped with redio altimeter, FCR 718, with an accuracy of  $\neq$  25 feet between 200 and 60,000 feet altitude over smooth terrain. Readings were taken from the radio altimeter at the time the plane came into the flight pattern for making the aerial photographs and any changes were noted. Passes were made at altitudes of 1,740, 1,700, and 1,750 feet.

Radiation has prevented making postshot depth survey; but this will be accomplished as soon as possible. Range poles will be placed at the end of the pre-surveyed Radii 2, 3, and 4 (Fig. 1.8-1), and transits will be sot up at the end of Radii 1, 5, and 6. An LCM or DUKW will enter the crater and lead line soundings, five per radii, will be made and the point of the sounding will be triangulated by the transits.

### PESULTS

Because residual radiation was high enough to prevent postshot survey, it is decided that a lead line sounding would be rade from a helicopter at oppreximately ground zero. A Rad-Safe survey flown at an altitude of 10 feet iss made at  $D \neq 11$  (1300 hrs 16 May 56) giving the results as shown in Fig. 1.2-2. On  $D \neq 12$  (17 May 56), a sounding was made from a helicopter which howered over ground zero at approximately 25 feet. The sounding made, corrected to the datum plane (6 inches below mean low vetor spring), gave the depth of the evator to be 45.4 feet. The survey took approximately 15 minutes for positioning the helicopter and making the sounding; persons exposed received zero vedication.

The postshot aerial photographs were studied; the diameter from rim to rim of the lip was estimated to be 430 feet.

#### CONCLUSIONS

No conclusions can be drawn until the findings of the film analysis and the lead line soundings have been made.



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LACROSSE-LAYOUT OF PRE SHOT SURVEY





LACROSSE, RAD-SAFE CRATER SURVEY 1300 HR - 16 MAY 56

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FIG. 1.8-2


Project 2.64 - FALLOUT LOCATION AND DELINEATION BY AERIAL SURVEY - R. Graveson

#### OBJECTIVES

To survey the gamma radiation from fallout contaminated lagoon islands, legoon water area and ocean areas using an aircraft borne detector. DESCRIPTION AND EXPERIMENTAL PROCEDURE

One P2V-5 aircraft was equipped with gamma radiation detectors to record the dose rate arriving through the thin aircraft skin from the surface below.

The aircraft starting approximately  $H \neq 3$  was to fly over all islams in the Eniwetok Atoll at an altitude of 300 feet, then survey the lagoon area to the west of IVOME. After survey of the atoll, the aircraft would continue source and survey over the open ocean to the neith and east, perhaps to a distance of 75 miles. During the flight, the activity observed by the aircraft was to be reported on a strip chart. This data would eventually be subject to earlysis in an effort to establish ground surface radiation contours.

During the survey of land surfaces, some special attention and possibly repeated passes were contemplated for the I4CROSSE crater.

A series of misunderstandings associated with the mechanics of filing flight plans and the purpose of the rission delayed the aircraft entry into the evon of interest for a period of 4 hours. Further confusion resulted in prohibiting the aircraft from flight lower than 1,000 feet and ordering it away from the atoll land areas. Rain squalls over the lagoon area presented an innediate possibility of aircraft contamination. All circumstances combined to withdrawing the mission without any data.



#### IACROSSE

Project 2.65 - ANALYSIS OF FALLOUT AND OF BASE SURGE - M. Morgenthau

#### OBJECTIVES

The general objectives of project 2.65 participation in REDWING were to: (1) obtain fallout samples on land and to perform radiophysical and radiochemical measurements on the samples; (2) prepare dose rate contours of the atoll area from information gathered by this project, other projects, and Rad-Safe; and (3) evaluate the role of the base surge in transport of radioactive material.

Project 2.65 had only limited participation in LACROSSE. The main purpose for this participation was to obtain dose rate contours near the crater. DESCRIPTION AND EXFERIMENTAL FROCEDURES

Stations at Emiwatok Atoll ware equipped with a Gross Fallout Collector (CFC).

On D day, D  $\neq$  1, and D  $\neq$  2, an varial survey of residual radiation was unde over the respective atolls by helicopter. The measurements were taken by means of a probe on a long cable suspended below the hovering helicopter. The position of the probe was determined by comparison with maps and aerdal photographs. STATION LOCATIONS

The instrumentation at the various stations is shown in Fig. 2.65-1.

Aerial Survey: Aerial survey readings taken on three successive days are plotted as a function of time in Fig. 2.65-2. The average slope of the field gamma-decay curves for the islands shown during the interval H  $\neq$  18 to H  $\neq$  50 hours is -1.3. The corrected dose rates and the corresponding H  $\neq$  1 hour values

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are given in Table 2.65-1. The H  $\neq$  1 hour values were determined using -1.3 as the gamma-decay exponent as determined from the curves of Fig. 2.65-2. The curvey points on YVONNE and WILMA are shown in Fig. 2.65-3 along with the corresponding H  $\neq$  1 hour readings. Fig. 2.65-4 shows the H  $\neq$  1 hour average dose rates for the seven islands surveyed.

Decay Data: Garma dose rate decay was determined by counting gross fallout samples with a Jordan Survey Meter mounted in a load pig for constant geometry. A typical gamma-decay curve is shown in Fig. 2.65-5. A typical betadecay curve is shown in Fig. 2.65-6.

Radiochemistry: Ground scoop samples were recovered from Sites WILMA and GENE. Another sample was retrieved from a depression in the canvas top **a** an abandoned truck at Site GENE. It was discovered that all the particles from the truck canvas were radioactive, while very few of the particles from the ground emples were radioactive. This observation, plus the opinion that it is improbable for particles other than fallout to be collected at the height of **a** improbable for particles other than fallout to be collected at the height of **a** improbable for the belief that this sample is representative of the fallout in that area. All of these samples were size greded into various size fractions, and radiochemical analyses for Np<sup>239</sup> and Mo<sup>99</sup> were performed on each fraction. From the analysis, the following conclusions were drawn:

1.  $Np^{239}$  fractionates with respect to  $No^{99}$  as a function of particle size. As shown in Table 2.65-2, the ratios of  $Np^{239}$  to  $No^{99}$  and the capture/fission retios, which are proportional to them, appear to decrease as the particle size of the sample increases. Even the lowest value, 0.14, is almost twice the 0.036 value reported by LASL for a cloud sample.

2. The individual contributions of Np<sup>239</sup> and Mo<sup>99</sup>, in relative units, to the total beta activity of the samples generally increase with increasing particle size.  $\sim$ 

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COPIEDJDOE LANL RC Microscopic observations of the fallout collected from the GENE truck ennous indicated at least two general types of particles. One type resembled intural coral, while the second was either partially or totally black. The black particles were ferromagnetic to varying degrees and gave positive qualitative tests for iron. The white particles were composed of both calcium carbonate and calcium hydroxide (or oxide). The hydroxide, or oxide, appeared to be uniformly distributed through the volumes of the particles. On the average, the black particles were individually about four times as radioactive as the white particles in the size fractions larger than 50 microns. The radioactivity of both types of particles appeared to be uniformly distributed through the volumes of the particles.

The bulk density of the samples from the Total Fallout Collector at Site WHMA and from the GENE truck targetlin was 2.66  $g/cm^3$ . The julk density of PARRY Island soil was found to be 2.70 - 2.75.

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# TAHE 2.65-1

-- CORRECTED AERIAL SURVEY READINGS - LACROSSE (FIELD GAMMA-DECAY FACTOR: -1.3)

| ISLAND | SURVEY<br>POINT   | TIME AFTER<br>SHOT (hr)  | CORRECTED<br>READING<br>(nr/hr)  | R/HR AT<br>H ≠ 1 HR.  | AVG H / 1<br>HR DOSE<br>RATE (r/hr) |
|--------|---|--|--|---|-------------------------------------|
| YVONNE | 2<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12         | 7.3<br>9.25<br>9.3<br>26.17<br>50.25<br>50.3<br>26.25<br>26.3<br>26.83<br>50.83<br>50.5<br>50.58 | 170<br>130<br>1700<br>2500<br>2000<br>14000<br>56000<br>45000<br>50000<br>15000<br>3800<br>760 | 2.2<br>2.3<br>30.6<br>175.0<br>328.0<br>2301.0<br>3920.0<br>3160.0<br>35000.0<br>2480.0<br>627.0<br>125.0 |                                     |
| WITMA  | 1<br>2<br>3<br>Grd rdg at<br>Grd rdg at<br>Grd rdg on<br>ocean side | 7.5<br>26.1<br>50.7<br>10.1<br>54  | 700<br>240<br>75<br>800<br>90  | 9.7<br>17.4<br>12.4<br>16.0<br>16.0   | 14.0                                |
| 2.011A | 1   | 7.25   | 150  | 2.0   | 2.0                                 |
| TTDA   | 1<br>2<br>3   | 7.58<br>26.0<br>50.58  | 5000<br>1100<br>350  | 69.0<br>75.0<br>58.0  | 67.0                                |
| PEARL  | 1<br>2<br>3   | 7.7<br>26.0<br>50.5  | 6000<br>1200<br>500  | 85.0<br>83.0<br>82.5  | 83.0                                |
| JANET  | 1<br>2<br>3   | 7.75<br>25.83<br>51.4  | 7000<br>1/400<br>530   | 98.0<br>95.0<br>90.0  | 94.0                                |
| CATSY  | 1<br>2<br>3   | 7.83<br>25.65<br>50.28   | 13000<br>2900<br>900   | 192.0<br>193.0<br>156.0   | 180.0                               |

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TABLE 2.65-2 JACROSSE CAPTURE/FISSION DATA

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| e '170 <b>7 D</b>  | PARTICLE<br>SIZE         | Np <sup>2,7</sup> /Mo <sup>77</sup><br>(Dist. Rate)<br>at | CAPTURE      |
|--|--------------------------|---|--------------|
|  | FRACTION                 | h – houn  |              |
| Piiraai (WILMA)<br>Ground Sample   | O— <u>≀</u> ; <i>1</i> ; | . 3.25  | 0.16         |
| dioting beipic   | 44-74                    | 3.09  | 0.16         |
|  | 74-105                   | 3,81  | 0.19         |
|  | 105-149                  | 3.20  | 0.16         |
|  | 149-210                  | 2.91  | 0,14         |
|  | 210-420                  | 2.78  | 0.14         |
| Teiteiripucchi (GENE)  | 0-44                     | 5.65  | 0,28         |
| Truck Canvas   | 1;1;-74                  | 6.29  | 0.31         |
|  | 74-105                   | <i>L</i> , 03   | 0.20         |
|  | 105–14 <b>9</b>          | 3.98  | 0,19         |
|  | 149-210                  | 3,05  | 0.15         |
|  | 210.420                  | 3.65  | 0, ]\$       |
|  | 420-840                  | 3.72  | 0,18         |
| a a a a a a a a a a a a a a a a a a a  | Total Solid              | 3.38  | 0,19         |
| Witeiripucchi (GRE)  | 0-5                      | 5 <b>.</b> 2 <b>3</b>                                     | 0.26         |
| Ground Sample  | 514                      | 5.08  | 0.25         |
|  | 10-22                    | 4.62  | 0 <b>,22</b> |
|  | 16-32                    | 4.70  | 0,2 <b>3</b> |
|  | 26-40                    | 5,10  | 0.25         |
|  | 40-50                    | 4.29  | 0.21         |
|  | 214- <b>74</b>           | 3.52  | 0.17         |
|  | 74-105                   | 3.62  | 0,18         |
|  | 105-149                  | 3.29  | 0.16         |
|  | 149-210                  | 3.78  | 0,18         |
| Real of the second descent second descent second descent second descent second descent descent descent descent | 210-420                  | 2.97  | 0.14         |
| Cloud Sample (Data   | 1                        |   | 0.086        |

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(HOURS 102 1000 TYPICAL LACROSSE & DECAY 100

FIG. 2.65-6

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Project 4.1 - FLASH BLINDNESS - Col. R. S. Fixott

#### CPJECTIVES

a. To gain information regarding the behavior of lid reflexes under the high illuminations produced by atomic devices; to further evaluate the blink reflexes as a protective mechanism against chorioretinal burns.

b. To gain information on shutter and filter mechanisms for eye protection against chorioretinal burns caused by atomic weapons of various types and yields.

### INSTRUMENTATION

The experimental arrangement for this project required the exposure of eminal eyes to the weapon detention at distances which produced retinal lesions in a similar test series during UPSHOT-ENOTHORE. Eabbits and monkeys were the animals of choice; the former because of ready availability and limited motility of the eye, the latter because of close resemblance to the human eye. Exposure racks were constructed to render nearly complete protection of the animal from whole body effects, when such protection was indicated. Direct exposure was limited to one eye of subject rabbits. The monkeys had both eyes exposed, being used solely for determining the protection offered by the blink reflex.

Staggered shutters of two types were used. The simple closure shutters were open at time zero and closed at varying intervals after, up to 1 second. The closed-open-closed shutters were closed at time zero, opened at a specified time, remained open for varying durations, then closed.

Prototypes of electromagnetic shutters of two types are being field tested as a part of this program. These shutters are designed to prevent or minimize temporary flash blindness, after-images, or retinal burns. Results obtained on animals exposed behind these shutters will be compared with those obtained by other shutters and filter mechanisms.

None of the animals exposed had eyes held open by artificial means. This introduced the possibility that the eye might be closed at time zero. An alarm bell was set up to waken animals. Cameras focused on the animals were used to determine shutter speed and to ascertain whether eyes were open during the time of exposure.

No arinals exposed to detonation LACROBSE received choricretinal Lurns.

#### CONCLUSIONS

Predicted total thermal yield at the exposure site on DAVID (Japtan), 8.9 miles from ground zero, should have produced eye datage. Lack of choricretinal burn injury may be explained by two factors:

a. Greater than expected attenuation of the thermal yield at the exposure site due to high water content of the air and salt water spray at the low exposure site level.

b. The obscuring of a significant portion of the fireball by debris raised by this surface burst.

Since no burns were produced on any of the exposed animals, no estimate of the effectiveness of the various protective mechanisms can be given. However, modification of projected future participation at Eniwetok based on these negative findings is planned. The lack of

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eye injury at this distance with this type weapon should then become significant as basic data.

#### AFFEDEX TO REPORT

Following detonation of LACRODE, the ophthalmologist then with this project (Capt. D.V.L. Brown) was asked to examine seven (7) persons thought to have observed the flash from the airstrip on FRED (Eniwetok) without eye protection. Their story indicates that the actual burst was at least partially obscured by a parked SA-16 type aircraft about 30 yards distant from them. All seven (7) complained of photophobia and headaches associated with seeing the sudden, brilliant light flash. None of them noted significant reduction in visual acuity. Dr. Brown noted questionable retinal edena on five (5) of the seven (7) but <u>no</u> definite retinal burn. These men, with one exception, were rechecked by Col. R. S. Fincit on 27 May 1956. Three still noted hee back and some photophobia, but visual acuity was not subjectively or objectively reduced. There was no evidence of eye injury attributable to the atoric weapon.



#### TAORO3SE

Project 5.3- In-Flight Participation of a B-66B Aircraft - R.W. Eachman

#### GRUEROTAVE

The primary objective of this test was to measure the gust effects of a low yield nuclear weapon on a B-66B aircraft in flight.

Instrumentation for the B-66 consist of the following: 57 strain Gages at 4 stations and 26 T.C. at 6 stations on L.H. wing, 16 strain gages at 1 station on the R.H. wing, 22 strain gages at 3 stations and 18 T.C. at 4 stations on the .H. horizontal stabilizer, 17 strain gages at 2 stations and 2 T.C. at 1 station R.H. horizontal stabilizer, 15 T.C. at 3 station on the L.H. elevator and 2 T.C. at 1 station on R.H. elevator, 26 channels of engine information, 16 calorimeters and 2 radiometers on tail and 1 colorimeter and 2 medicreters in fullage belly, 3 pressure pickups on the wing 3 on a pennage and at 7 stations on fuselage, 16 accelerometers, 8 circelation channels, a photo recorder covering 32 basic flight and engine pennage instruments together with 8 indicator lights, 3 motion picture cameras recording wing and tail deflections.

#### A RCRAFT POSITION IN SPACE

The ship's aircraft electrical system failed giving the crew none of its normal flight instruments just prior to the run into the target at H-hr. The crew found that they could not maintain a good position and altitude on emergency instruments alone and made an early abort placing them considerably beyond a test condition.

RESULTS

As a result of the abort, the aircraft received no data.



#### TACROSSE

Froject 5.4 - In-Flight Participation of a B-57B Aircraft - 1st It. H.M. Wells

#### CRUPOTIVE

The objective of this test was to reasure the effects of a nuclear detonation on an in-flight B-57B aircraft weapon system.

#### ANSTRUMENTATION

Out of 220 channels being recorded, 20 data channels were lost for writing reasons. They have been repaired, or replaced by spares.

#### AIRCRAFT POSITION IN SPACE

The JB-57B was flying at an absolute altitude of 14,500 feet, heading 135° in a teil-on position at H-hr. Slant range to ground zero at H-hrinas 15,021 feet (aircraft traveling at 863 ft/sec). Aircraft position at time of abook arrival (H/26.2 seconds) was 28,570 feet slant range at same heading ind altitude as at H-hr.

RESUITS

Thereal: Total thereal energy resoured was 1.14 cal/cm<sup>2</sup>.

Gust: Total gust load at this of shock arrival was 1.094 g's (35% of allowable limit).

Overpressure: Peck overpressure masured was .32 psi at E/26.28 sec.

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Froject 5.5 - IN-FLIGHT PARTICIPATION OF F-84F AIRCRAFT - Captain R. F. Mitchell

#### CEJECTIVE

The objective of this project was to detentine the response of the F-24F weapon system when exposed during flight to the effects of a nuclear detonation. INSTRUMENTATION

Instrumentation of the F-84F aircraft on LACROSSE was as follows:

1. Waiter (Capabilities F-84F) - Instrumentation of primary concern consisted of 35 strain gages for recording gust response located at three right wing stations, one left wing station, two fuselage stations, two right stabilator stations, and one left stabilator station. Correlative instrumentation consisted of everpressure gages at fuselage Station 75, in addition to time zero fiducial signal, radiometer, and calorimeters located at Station 80, botto while of the fuselage.

2. Barkey (Sideloads F-34F) - The instrumentation consisted of strain ( ge bridges located at Station 90 and 150 on left and right wing; Station 365 on the fuselage; Flight Station 12 and 35.5 on the left and right stabilizer and Waterline Stations 20 and 53 on the fin. The forementioned strain gage bridges yield ed bending noment information. Structural responses were related to emergy inputs with overpressure transducers located on a nose boom and in the sides of th fuselage. A total of 100 channels of information were capable of being recorded AIRCRAFT POSITION IN SPACE

1. Waiter - The planned position of Waiter was on an in-bound heading of  $050^{\circ}$ T with no horizontal offset, to be 8,800 feet from ground zero at T<sub>o</sub> and ov ground zero at H  $\neq$  8 seconds. The speed on the final run was to be 800 ft/sec.





2. Barley - The planned position of Barley was on an in-bound heading of  $050^{\circ}T$  with a horizontal offset of 22,300 feet left of ground zero, to be 15,100 feet abreast of ground zero at H  $\neq$  19 seconds. Actual position on shot day was 3.25 seconds early and 640 feet left of course at T<sub>o</sub>; 1.15 seconds early and 430 feet to left of course at shock arrival, altitude was 10,180 feet.

RESULTS

1. There was no apparent aircraft or instrumentation damage to either sir-

2. Data obtained:

a. Waiter received an overpressure of 0.8 psi, thereas 1.0 psi the prodicted for the positioning yield. The critical wing bending the statutes that 50 percent of design limit. A refined value will be available when the creat distribution of wing fuel is determined. Since aluminum skin temperature rises that not of primary importance in this shot, it was not reduced as priority data in the field.

b. Parley was deprived of citaining 50 percent of its data due to the recording speed of one of its two 50-channel cacillographs being set at one inch per second. This miss-setting caused the traces to be jumbled up to the extent that data reduction was virtually impossible. Steps have been taken to provent miss-settings such as this in the future.

# Project 5.6 - IN-FLICHT FARTICIPATION OF AN F-101A ALRCRAFT - Captain M. H. Lewin

#### OBJECTIVE

The objective of Project 5.6 is to determine the responses of an in-flight F-101A aircraft to the thermal, blast, and gust effects of a nuclear detenation. A correlation of the responses, combined with known characteristics of any weapon, will be used to define the maximum safe delivery capability of the aircraft.

#### INSTRUMENTATION

The aircraft was instrumented with radiometers, calorimeters and pressure transducers to measure the thermal and blast inputs and with strain gages, thermocouples and various other instruments to measure the aircraft responses to the imputs. For LACROSSE shot, the aircraft was positive added to there aliced by receive 80% design limit distributed up load on the stabilator based on the positioning yield.

#### AIRCRAFT POSITION IN SPACE

The aircraft was to fly at 12,000 feet absolute altitude on an in-bound heading of  $135^{\circ}T$  at a speed of 800 fps TAS. It was planned that the elicitat would arrive over ground zero at  $T_{\circ}$  with shock arrival occurring 11 sectors later at a horizontal range of 8,800 feet. Actual shot day position was 140 feet abeam of ground zero at  $T_{\circ}$  with shock arriving 12.45 seconds later at a horizontal range of 10,500 feet.

#### RESULTS

1. Damage: There was no evident damage to the aircraft.

2. Instrumentation: No evident damage to the instrumentation was noted. Of the 50 oscillograph recorded parameters, 48 produced usable data. A standby

- 51 -



shear gage was drifting, producing unreliable readings and an accelerometer went off the paper and was unreadable, although functioning properly. One wing deflection camera jauned and produced no results. The photo panel camera, recording 26 parameters, vibrated excessively at shock arrival and five frames (.312 seconds) were unreadable. It is felt that no data was lost however, since the instrument was not sensitive enough to react in .312 seconds.

3. Gust Data: Overpressure measured was .75 psi. Gust response was about 40 percent of design limit load on the stabilator. Eased on the announced yield, the responses were generally less than would have been expected. This indicates some conservatism in the selected position.

4. Thermal Data: Thermal response was considerably less than experted. A A T averaging 50°F on the honeycomb surfaces was recorded; this can be compared to a A T of 240°F expected. Based on the measured inputs, the temperature rises capatived on the critical components were about 15 readent low. Weis also indicates some conservatism in the selected position.

5. Nuclear Radiation: A reading of .585 REM was taken from the pilot's film bedge and can be compared to a .81 REM prediction based on the actual yield and position. Again, some conservatism is indicated.

6. General: The participation was considered highly successful by this project. The responses recorded were of sufficient magnitude to serve as a basis for a re-positioning of the aircraft on further shots.

#### DISCUSSION

The contents of this postshot report are preliminary, tentative and approximate. They are subject to change pending further evaluation of the data collected. They were reported at this time to provide early test results to those concerned with effects of nuclear weapons. 51

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Froject 5.7 - Thermal Flux and Albedo Measurements from Aircraft -

Capt. R. L. Dresser

#### O-J-OTIVE

The objective of this shot was to obtain thermal flux and albedo information of a nuclear detonation with airborne calorimeter, radioeters, and sixteen mm. motion picture cameras.

#### INSTRUMENTATION

Instrumentation within the purview of Project 5.7 which was installed in the B-57 included nineteen (19) NRDL calorimeters and two (2) NRDL radiometers for measuring the direct and surface reflected thermal radiation. These instruments possessed various fields of view and were suitably filtered to obtain qualitative spectral distribution information. Six (6) GSAP N-9 comeras were utilized to obtain photographic coverage of the fireball, the curth's surface, and of shouts beneath the aircraft. Two (2) of the cameras oriented towards owound zero were equipped with spectroscopic attachments to obtain entinuous spectra in the visible region. Of the other two (2) tail position cameras, one camera had a blue filter and the other had a red wilter for the purpose of obtaining pictures at both extremes of the visible region of the spectrum. The remaining two (2) cameras were oriented vertically for the purpose of obtaining photographic coverage of the earth's surface and of clouds beneath the aircraft.

Instrumentation installed in the B-66 consisted of the basic twenty-one (21) thermal instruments, and twelve (12) cameras.



#### ATRORAFT-POSITION IN SPACE

Information of the position in space of each aircraft is contained in the

Project 5.3 - B-66

Project 5.4 - B-57

#### I-SULTS

Thermal: The very preliminary values of total thermal input to the aircraft obtained on Project 5.7 instrumentation are included in the postshot reports of the appropriate project indicated above.

Photographic Data: Of the eighteen (18) cameras under the purview of Project 5.7, twelve (12) obtained no results because of the abort of the B-66. These films were destroyed. Of the six (6) cameras in the B-57, the red filtered tail compra suffered film breakage and obtained no pictures. This film was destroyed. A prevently represently poind results were obtained with the remaining files (5) excerts. The two (2) cameras equipped with the spectroscopic attachment, which were located in the EC&G "ELMER" photo tower, also apparently obtained good re-

#### Film Surmary:

| to ber of       | Number of magazines com | Number of ragazines | Number of magazines |
|-----------------|-------------------------|---------------------|---------------------|
| Agazines loaded |                         | for analysis        | destroyed           |
| 20              | 20                      | 7                   | 13                  |





#### LACRO35E

#### Project 6.1 - ACCURATE LOCATION OF ELECTROMACRIETIC PULSE SOURCE - Dr. E. A. Lewis

#### OBJECTIVE

To utilize the electromagnetic signal originating from nuclear weapon detonations to determine ground zero of detonation. Secondarily to obtain the yield data that is available in the bonb pulse.

#### PROCEDURE

Location of Ground Zero is made by use of an inverse Loran principle. The exact time the bonb pulse is received at various stations is recorded. The exact time difference in receipt of the electromagnetic pulse between two stations will be used to determine a hyperbolic curve which runs through ground zero. The point of intersection of two or more curves determines ground zero.

There are two systems. One of the system as the long base line system and the other, the short base line system. Each system has two rets of stations. The long base line has one set of stations located in the Havailan Islands (Midway, Palayra and Maui) with synchronizing antenna station at Haibu, Maui, and the other set of stations in the States (Harlingen, Texas; Blytheville, Aukansas; Kinross, Michigan and Rore, New York) with synchronizing antenna station at Cape Fear, North Carolina. The short base lines have one set of stations located in the Hawaiian area (Kona, Hawaii; Fapa, Hawaii; and Red Hill, Maui) the other set in California (Fittsburg, Woodland, and Maryville).

FESULTS

1. Short base line in Hawaii recorded bomb pulse.

2. Short base line in California recorded bomb pulse.

3. Long base line in Hawaii recorded bomb pulse.

- 55 -



4. Long base line in States reported equipment failure.

5. Griffiss AFB experienced time synchronization difficulty.

# CONCLUSIONS

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No conclusion can be made until further information is received from data reduction and interpretation.

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Froject 6.3 - EFFECTS OF ATOMIC EXPLOSIONS ON THE IONOSPHERE - Major Mathew Hawn

#### CEJECTIVE

The objective of Project 6.3 is to obtain data on the effects of high yield nuclear explosions on the Ionosphere. Principally, to investigate the area of absorption, probably due to the high altitude radicactive particles, and to study the effect of orientation relative to the earth's magnetic field on F2 layer effects.

#### JNSTRUMENTATION

The system comprises:

1. Two Ionosphere recorders, type C-2, operating on pulse transmission, installed in 6 ton trailer vans, one located at Rongerik Atoll and one located at Mesaie in the Caroline Islands.

2. One Jonosphere recorder, type C-3, operating on pulse transition, installed in a C-97 plane based at Eniwetok Island.

Detailed Description:

1. Ionosphere recorder site (Rongerik Atoll)

site (Kusaie)

a. AN/CPQ-7, type C-2 Ionosphere recorder with a power output of 10 KM peak pulse alternately transmitting and receiving automatically over the range of Coopencies from 1 to 25 mogacycles. This equipment more uses and records at vertical incidence the virtual height and critical frequencies of ionized regions of the upper atmosphere.

b. A 600 ohm multiple wire antenna designed and erected, so that the direction of maximum intensity of radiation will be at the desired vertical angle



2. Ionosphere recorder site (C-97 airplane)

a. Same as for Rongerik and Kusaie, except that a C-3 Ionosphere recorder was used. This recorder is the same as the C-2, except for a few modifications and improvements.

b. The transmitting antenna in the C-97 was a single wire delta fastened to the lateral extremities of the tail assembly.

#### OFERATIONAL

Ground stations at Rongerik and Kusaie, using 15 second sweep, operated on normal 24 hour schedule, 5 sweeps per hour until H-15 minutes; thence continuous watil H / 1 hour; thence routine operation.

#### FLIGHT PLAN FOR C-97 AIREORNE STATION

Plane remained on ground at Eniwatok for LACROSSE.

All stations operated successfully during this test.

An examination of the film records for LACROSSE indicates that normal conditions existed within the Ionosphere during L-day. There were no mobiciable effects on the Ionosphere from Test LACROSSE.



Project 6.4 - Determination of Characteristics of Airborne Flush Mounted Antennas and Phototube for Yield Determination at Extended Ground to Air Ranges - A. J. Waters

#### OPJECTIVES

1. To determine the effectiveness of flush mounted airborne antennas and phototubes at various ground-to-air ranges in detecting characteristic low frequency electromagnetic radiation and visible radiation, respectively.

2. To determine the temporal and amplitude characteristics of the low frequency electromagnetic radiation at various ground-to-air ranges.

3. To determine the temporal and intensity characteristics of visible radiation at various ground-to-air ranges.

4. To determine the effects of ambient conditions upon the satisfactory measurement of the parameters specified in items 1 and 2 above.

#### INSTRUMENTATION

| 2 | fiducial antennas | 2 | scope cameras   |
|---|-------------------|---|-----------------|
| 1 | whip antenna      | 1 | sequency canera |
| 1 | synchronizer      | 1 | recorder        |

2 photoheads

```
2 DuMont Scopes (1 a dual beam, 1 a single beam)
```

#### TECHNIQUE

Signal is received by antenna fed through an amplifier and then to the scope. The signal is then photographed. Photohead output is led directly to the recorder. The sequence camera photographs the blast directly for use in correlation of previous data. Distance was approximately 13 miles.

#### RESULTS

No discernable signal could be seen in the photograph.

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#### IACEOSSE

Project 8.1 - Easic Thermal Radiation Measurements - W.B. Plum OBJECTIVE

The principle objective of Project 8.1 was to measure the irradiance as a function of time, thermal radiant energy, and the spectral distribution of the thermal radiant energy from a kiloton-range surface burst and compare these data with corresponding data from tower shots.

#### INSTRUMENTATION

The NRDL radiometer and the NRDL calorimeter with appropriate filters were used to measure the thermal radiation at Station 815.01 (8,121 ft from GZ) on YVONNE and at Station 812.02 (14,392 ft from GZ) on WILMA. The data were recorded on Heiland oscillographic recorders, two of which were placed at each station. Each recorder gave a time history plot for wach of the following instruments:

- (1) Total energy, quartz filter, 90 degree field of view
- (2) Total energy, quartz filter, 90 degree field of view
- (3) Spectral, 3-69 filter, 90 degree field of view
- (4) Spectral, 2-58 filter, 90 degree field of view
- (5) Spectral, RG-8 filter, 90 degree field of view
- (6) Spectral, 7-56 filter, 90 degree field of view
- (7) Field of view, quartz filter, 11 deg field of view
- (8) Field of view, quartz filter, 22 degree field of view
- (9) Field of view, quartz filter, 45 degree field of view
- (10) Field of view, quartz filter, 90 degree field of view
- (11) Field of view, quartz filter, 160 degree field of view
- (12) Radiometer, quartz filter, 90 degree field of view

- 60 -



The instrumentation for the second recorder at each station was identical with the first recorder system with the exception of an 0-52 filter on channel 3 and a Germanium filter behind a 7-56 filter on channel 5. The first 11 instruments were calorimeters and the 12th instrument was a radiometer. Aiming point cameras were used to photograph the detonation. All of the instruments gave data and two of the four cameras, one at each station, functioned satisfactorily.

#### RESULTS

A preliminary analysis of the data in the field indicates that the energy received at the YVONNE station is low relative to the energy received at the WIIMA station. This reduction in energy was, no doubt, due to the fact that the soil was loose and could be stirred up by the blast and thermal radiation, thus obscuring the latter portion of the thermal pulse. A more careful examination in the laboratory of the storry delivered as a function of time will be required in order to envive at a reasonable transmission coefficient for the two paths. The preliminary data, reduced without the aid of precision instruments, are as follows:

| STATION | QUANTITY MFASURED      | QUANT ITY                          |
|---------|------------------------|------------------------------------|
| 815.01  | Total Energy           | $1.8 \neq 0.3 \text{ cal/cm}^2$    |
| 815.01  | Maximum Jeradiance     | $4.5 \neq 0.7 \text{ cal/cm}^2$    |
| 815.01  | Time of Max Irradiance | 0.19 seconds                       |
| 812.02  | Total Energy           | $1.2 \neq 0.2 \text{ cal/cm}^2$    |
| 812.02  | Maximum Jeradianoe     | 1.9 £ 0.3 cal/cm <sup>2</sup> /sec |
| 812.02  | Time to Max Irradiance | 0.21 seconds                       |

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Project 8.5 - AIRBORNE HIGH RESOLUTION SPECTRAL ANALYSIS - Dr. Ralph Zirkind

#### OBJECTIVE

To determine the radiant power of a 30-40 kiloton surface burst as a function of wavelength and the fireball color temperature as seen from an airborne station. These objectives were to be accomplished by determining the atmospheric attenuation by an independent measurement and correcting the power received at the instrument station aboard the aircraft.

#### DESTRUMENTATION

The spectral distribution of the radiant power is obtained from a medium quartz Milger spectrometer. The spectrum is sampled in marrow bonds by photopells in the widthle region and PS calls in the information. The electrical signal is then recorded on an Ampex 814 tage recorder, with a resolution time of 150 A sec. The transmission measurement is accorplished by baseding a pulsed light signal of boost output and spectral distribution from a fixed point on the ground towards the aircraft. The attenuated beam is received by a detector in the aircraft and recorded on a Heiland recorder. The detector consists of two filtered photomultiplier tubes compling two spectral regions, (1) .3-.55 microns and (2) .6-1.05 microns. In addition, a quartz filtered calorimeter, 22 degrees field of view, is utilized to measure the approximate radiant exposure received at the spectrum view. RESULTS

The aircraft was located at the intended position (within 600 feet). (Planned position at H-hour was on an inbound heading of 135<sup>o</sup>T with no horizontal offset to be abreast of ground zero at H-6.5 seconds with a horizontal range of 5,000 feet

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The <u>spactrometer</u> operated normally and to date, data has been obtained on 7 of the available 13 channels. It is possible, additional data exist on the penainder.

The calorimeter functioned and satisfactory data was obtained.

The light-source for transmission measurements failed to operate on D-day and consequently, no data have been obtained. Extrapolated data from simulated runs on ERIE event will be used in the final analysis.

DISCUSSION

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The extent of noise within the various tape channels has required a detailed filtering process. Consequently, the final data reduction will be accomplish ed in the laboratory where suitable filters will be exployed. This applies to all subsequent events.

As will be noted here and subsequent participations, accorde positioning out be according by radar observations and a wightional calculations.

Delay in data reduction has been caused by the fact that Project 8.5 was to utilize the tape play-back unit of Project 8.1 to conserve funds. This may t that no data processing was possible prior to ZUNI plus three days.



Froject 9.1 - TECHNICAL PHOTOGRAPHY - Lieutenant Colonel Jack G. James

Three R3-50 aircraft participated on this event, CARTER 1, 2, and 3. Aircraft were positioned at 20,000 feet, 70 nautical miles from Ground Zero, in the Nest, South and East quadrants. Each aircraft carried a camera assembly consisting of a 70mm cloud camera, a 35mm Eclair notion picture camera and a 16mm GSAP camera with a color load. All three cameras were mounted in an A-28 Gyro Mount. This mission was, for all practical purposes, a test run for air crews and equipment. Time of arrival for positioning purposes was excellent. Navigation to determine known positioning every two minutes was better than previously expected. All cameras, with the exception of one Eclair, operated without malfunction. Ero-determined exposure data for the Tri-X Gilm in the 70mm cloud eccents is in super by approximately 1 f Stop opening, but results are still measurable. Figerton, Cercleshausen, and Grier, Inc. enticipates fair analysis from ell mogatices. At conclusion of the cloud survey mission, CARTER 1 entered the crater area at plus 1 hour and made three controlled mapping runs over the crater. Republics from this photography were excellent.

Note: 9.1 photos are non-pictorial. Negatives have been sent to Poston for enalysis and are not available for postshot report.

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PART III

TACK UNET 1

# LASL PROGRAMS

KeithBy Keith Boyer Advisory Group

| Frojrem 10 - | - Thermal Radiation and Hydrodynamics                               | Н. | Hoerlin    |
|--------------|---|----|------------|
| Program 11 - | - Radiochemistry  | G. | Covan      |
| Program 12 - | - External Neutron Measurement and<br>High Energy Salma Measurement | R. | L. Asibodt |
| Program 13 - | - Fission Reaction Measurements                                     | J. | S. Malik   |
| Program 15 · | - Photo-Fhysics   | G. | L. Felt    |
| Program 16   | - Physics & Electronics & Reaction<br>History                       | в. | E. Natt    |
| Program 18   | - Thernal Radiation   | Н. | Hoerlin    |

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- 65 -

Project 10.1 - FIREBALL HYDRODYNALICS - J. Mullaney

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H. Hoerlin

The hydrodynamic yield **DELETED** was determined on the basis of three Eastman films each from photo stations at Farry, at the southern tip of Runit and from Piiaarai.

Three different methods of data reduction were employed, all of which are based on equation 17 of Chapter 5, by Bethe, in LA-1021, which states that the yield is proportional to the mass of the air engulfed, and the square of the shock velocity. The Bethe-Fuchs mass-correction terms were included.

More specifically, the first method, as employed by Joe Mullaney uses equation 17 and the mass-correction term in an integrated form. The propertionality factor was chosen to give agreement with the "older" pro-JEAPOT podicchamical yields. The resulting data are shown in column 2 of Table 10.1-1 (Integral Method).

The second method, as employed by Roy Blumberg, determines the yield from equation 17 on a point by point basis, also with mass-correction. The velocities were derived graphically from the RO&G radius-time data and the  $f(\sigma -1)$  function was obtained from KING shot, taking 540 KT as its yield. For data see column 3 of Table 10.1-1 (Differential Method).

Finally, the Mach-number scaling method was used by Roy Blumberg in a similar fashion as during TEAPOT, however, applying also mass-correction. The basic 1 KT Mach-number relation used is one worked out by D. Seacord and Tod Snyder utilizing TEM problem M and CASTLE data. See data in column 4 of Table 10.1-1 (Mach Scaling).

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TABLE 13.1-1

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Fig. 15.1<del>.</del>2

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Fig. 15.1-3

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> Frank Harrington Gordon Milne Marion Shuler Harold Stewart

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It is a preliminary report which describes the results of experiments planned and executed by many people from NRL (Stewart, Hanson, Harrington, Duttrey, Fussell, Weedman, Wall, Shuler, Duiley, Carpenter and Westfall), University of Rochester (Milne, Putman, Fyer), LASL (Ogle, Hoerlin, Skumanich, Shaw, Williamson, Deal and McQueen).





#### TABLE 18.1-1

WAVELENGTHS OBSERVED ON DATA FATH

102 SPECTROGRAPH (/10A)

| $\lambda_{-}$ | DESCRIPTION | λ_           | DESCRIPTION |
|---------------|-------------|--------------|-------------|
| 53 <b>91</b>  | W           | 3350         | S           |
| 501 <b>0</b>  | VW, Diffuse | 3234         | М           |
| 47 <b>57</b>  | S           | 3150         | VS – B      |
| 464 <b>8</b>  | М           | 310 <b>5</b> | L           |
| 11.25         | L           | 309 <b>2</b> | VW          |
| 433 <b>2</b>  | W           | 3034         | М           |
| 4138          | VW?         | 300 <b>3</b> | М           |
| /110          | VW?         | 293 <b>8</b> | MB          |
| 3 <b>332</b>  | М           | 295 <b>3</b> | VW          |
| 3370          | S           | 29/ <b>2</b> | V. <b>?</b> |
| 31.36         | L           | 290 <b>8</b> | I.B         |
| 3445          | VW          |              |             |

#### CODE:

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| S | Strong |
|---|--------|
| М | Medium |
| L | Light  |
| W | Weak   |
| В | Broad  |
| V | Very   |

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#### TATE 13,1-2

WAVELENGTHS OBSERVED ON MOVITOR FATH, AND SOME COMPARISONS

| 10 <b>2</b><br>∡ 10 <b>A</b> | U. of R.<br>∠2A | Descrip<br>tion | Ca   | Al    | Fe(raies<br>ultimes) |
|------------------------------|-----------------|-----------------|--|-------|----------------------|
| <b>.</b>                     | 4321            | SC              | 14318 (20 <b>)</b>                         |       |                      |
|                              | 4310            | SC              | 14308 (20)                                 |       |                      |
| 1308                         |                 | W               | 1430 <b>8 (</b> 20 <b>)</b>                |       |                      |
|                              | 430 <b>3</b>    | SC              | 1430 <b>3 (25)</b><br>14298 (18)           |       |                      |
|                              | 4291            |                 | 14289 (20 <b>)</b>                         |       |                      |
|                              | 4284            | WC              | 1428 <b>3 (20)</b>                         |       |                      |
| 4246                         |                 | W               | 424 <b>8 (10)</b><br>14240 (10)            |       |                      |
|                              | 422 <b>7</b>    | 1               | <u>14226</u> (50)                          |       |                      |
| /216                         |                 | L               |  |       |                      |
|                              | 4215            | W               |  |       |                      |
|                              | 4201            | W               | 4207 (10 <b>)</b>                          |       |                      |
| 13 <b>92</b>                 |                 | VW              |  |       |                      |
|                              | 4192            | W               |  |       |                      |
|                              | 418 <b>5</b>    | VW              |  |       |                      |
| 1164                         |                 | М               |  |       |                      |
|                              | 4129            | SD              |  |       |                      |
| <u>41</u> 28                 |                 | М               |  |       |                      |
| 40 <b>90</b>                 |                 | W               |  |       |                      |
|                              | 407 <b>9</b>    | SC              |  |       |                      |
| 400 <b>8</b>                 |                 | М               |  |       |                      |
| 4984                         |                 | VS              |  |       |                      |
|                              | 3%8             | ٧S              | 1397 <b>3 (15)</b><br>11396 <b>8 (</b> 500 | )     |                      |
|                              | 396 <b>2</b>    | W               |  | 13961 | (2000)               |
| 3 <b>%0</b>                  |                 | М               |  | 13961 | (2000)               |

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TABLE 18.1-2 (Contd)

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|                       | 102<br>/ 10A              | U. of R.<br><u>∕</u> 2A | Descrip<br>tion | Ca                            | Al                   | Fe(raies<br>ultimes)             |
|-----------------------|---------------------------|-------------------------|-----------------|-------------------------------|----------------------|----------------------------------|
|                       | a in ann an an an Anna An | 3945                    | C               | I3949 (15 <b>)</b>            | 13944 (1000 <b>)</b> |                                  |
|                       |                           | 393 <b>7</b>            | С               |                               |                      |                                  |
| •                     |                           | 393 <b>2</b>            | VSD             | 11393 <b>3 (</b> 600 <b>)</b> |                      |                                  |
|                       |                           | 390 <b>2</b>            | W               |                               | 113900 (200)         |                                  |
|                       | 339 <b>0</b>              |                         | М               |                               |                      |                                  |
|                       | 337 <b>0</b>              |                         | М               |                               |                      |                                  |
|                       |                           | 3859                    | SD              |                               |                      | - 1                              |
|                       |                           | 335 <b>3</b>            | SD              |                               |                      |                                  |
|                       |                           | 373 <b>7</b>            | S               | 113737 (50)                   |                      | `                                |
|                       | 3730                      |                         | MB              |                               |                      | (3735)                           |
|                       | 3714                      |                         | MB              |                               |                      | (3739 <b>)</b>                   |
|                       |                           | 3706                    | S               | 113706 (40)                   |                      |                                  |
|                       | 365 <b>6</b>              |                         | VW              |                               | 113655 (100 <b>)</b> | •                                |
|                       | 364 <b>0</b>              |                         | VW              | 13644 (15)                    |                      |                                  |
|                       |                           | 36 <b>33</b>            |                 |                               |                      |                                  |
|                       | 36 <b>16</b>              |                         | W               | 13624 (15 <b>)</b>            |                      |                                  |
|                       |                           | .3612                   |                 |                               |                      |                                  |
|                       |                           | 360 <b>3</b>            |                 |                               |                      |                                  |
|                       | 3596                      |                         | М               |                               |                      |                                  |
|                       |                           | 358 <b>5</b>            |                 |                               | 113537 (500 <b>)</b> | (3531 <b>)</b><br>(3570 <b>)</b> |
|                       |                           | 3521                    | W               |                               |                      |                                  |
|                       | 347 <b>6</b>              |                         | W               |                               |                      | (3475 <b>)</b>                   |
|                       |                           | 3465                    |                 |                               |                      | (3465)                           |
| ★ P ≠ 1 ≤ 1           | 3238                      |                         | VW              | 13361 (10)<br>13350 (10)      |                      |                                  |
| COPIED/DOE<br>LANL RC | 3224                      |                         | ٧W              | 13226 (10 <b>)</b>            |                      |                                  |

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#### TAFLE 13.1-2 (Contd)

|              | •               | - ·             |                      |                              | Fe(raies |
|--------------|-----------------|-----------------|----------------------|------------------------------|----------|
| 102<br>∠ 10A | U. of R.<br>£2A | Descrip<br>tion | Ca                   | A1                           | ultimes) |
| 3194         | ,               | L               |                      |                              |          |
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|              | 3180            | D               | 113179 (400)         |                              |          |
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|              | 3160            | D               | 113159 (300 <b>)</b> |                              |          |
| 3104         |                 | VW              |                      |                              |          |
| 308 <b>8</b> |                 | VW              |                      | 13092 (1000)<br>13082 (1000) |          |
| 301 <b>0</b> |                 | VW              | •                    |                              | (3020)   |
| 29 <b>96</b> |                 | WV              | 13000 (10)           |                              |          |
| 290 <b>0</b> |                 | W               |                      |                              |          |
| 2338         |                 | WV              |                      |                              |          |

#### CODE:

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| S | Strong                 |
|---|------------------------|
| М | Mejium                 |
| L | - Light                |
| W | Weak                   |
| С | Short Duration         |
| D | Long Duration          |
| В | Broad                  |
| V | Very                   |
| 1 | Fuzzy, possibly double |

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Fig.

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### PART IV

#### TASE UNIT 4

### SC PROGRAMS

E. I. Jenterins GTU-4

J. H. Scott R. Heppelvhite

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ONTRO/DUE F TAUL R**3**  Program 30 - Vulnerability Program 31 - Microbarography

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#### LACROSSE

Project 31.1 - Microbarograph - W. A. Gustafson

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The purpose of this project was to measure winds in even layer of the atmosphere. This was accomplished by measuring at neveral sites the arrival times of the shock wave reflected from the evene layer. Five sites were operated: Ujelang, Notho, Rongerik, Etkini, and Eniwetok. At each site two stations were operated about one mile apart. The difference in arrival times gives the angle of incidence of the shock and information from several stations way be combined to give the winds.

On lawyorse shot good records were obtained from all stations but no vind velocities are yet available.

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